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On Output Regulation in Systems with Differential Variational Inequalities

Aneel Tanwani, Bernard Brogliato, Christophe Prieur

Abstract—We consider the problem of designing state feedback control laws for output regulation in a class of dynamical systems which are described by variational inequalities and ordinary differential equations. In our setup, these variational inequalities are used to model state trajectories constrained to evolve within time-varying, closed, and convex sets, and systems with complementarity relations. We first derive conditions to study the existence and uniqueness of solutions in such systems. The derivation of control laws for output regulation is based on the use of internal model principle, and two cases are treated: first, a static feedback control law is derived when full state feedback is available; In the second case, only the error to be regulated is assumed to be available for measurement and a dynamic compensator is designed. As applications, we demonstrate how control input resulting from the solution of a variational inequality results in regulating the output of the system while maintaining polyhedral state constraints. Another application is seen in designing switching signals for regulation in power converters.

I. INTRODUCTION

Differential variational inequalities (DVI) provide a mathematical framework to model evolution of state trajectories which, in addition to ordinary differential equations, satisfy some algebraic relations as well. Roughly speaking, DVIs comprise an ordinary differential equation to describe the motion of the state variable, and a *variational inequality* (VI) that expresses the constraints, and relations that must be satisfied by the state variable. VIs are most commonly encountered in optimization, and DVIs have found applications in modeling of electrical circuits with nonsmooth devices, and mechanical systems with impacts.

While most of the work on DVIs in the recent past has focused on studying the solution theory of such systems [5], [7], [8], [21], some classical control-theoretic problems such as stability [9], [16], optimal control [4], observer and controller design [6], [17], [23] have been investigated in related system classes. The problem of output regulation for such systems, which relates to designing control laws for asymptotically tracking a reference trajectory or rejecting disturbances while respecting the relations imposed by system dynamics, was introduced in our recent work [25] and in this paper, we extend our results to a broader class of systems.

In the standard formulation of VIs [13], we consider a set-valued map, say F , and are interested in solving the

following inequality:

$$\langle F(v), v' - v \rangle \geq 0, \quad \forall v' \in \mathcal{S},$$

for some closed, convex, and stationary set \mathcal{S} . In the dynamical systems considered in this paper, we couple such VIs with ordinary differential equations, and moreover also let the set \mathcal{S} be time-varying.¹ Since the solutions of VIs could be abstractly represented using a set-valued operator, different tools from the theory of differential inclusions could be used to study the solutions of DVIs. We refer the reader to a recent paper [21] for results and literature in this direction. In this paper, we also propose results on existence and uniqueness of solutions for a particular system class, which is based on the theory of evolution equations with *maximal monotone* operators [3]. While VIs essentially describe a *maximal monotone* operator, in many practical systems, these operators only appear after certain linear transformations, and it is not evident that such transformations preserve maximality, or even monotonicity. Our approach extends the work of [5] by relaxing certain assumptions (that describe the transformation) required to show the existence of solutions. In a recent paper [10], it is shown that if the transformation matrices satisfy certain LMI (related to the passivity assumption in control theory), then maximal monotonicity is preserved. We generalize the results of [10] by considering nonlinear globally Lipschitz vector fields in system description, and consider nonstationary sets \mathcal{S} . The proof worked out in this case is also completely different than the work of [10].

The second main contribution of this paper comes in applying these results to study the problem of output regulation. Our approach is based on the pioneering work of [14] which proposed simple algebraic criteria for output regulation in multivariable linear time-invariant (LTI) systems. In [14], it is assumed that the plant under consideration is driven by the output of an LTI exosystem that models the dynamics of the reference trajectories and/or disturbances. Intuitively speaking, the proposed control input that achieves the output regulation comprises a feedback component to make the closed-loop dynamics stable and an additional open-loop component that shapes the steady state of the plant. The derivation of the open-loop component of the control input requires the exact knowledge of the exosystem dynamics, and hence the approach is termed as *internal model principle*. A large amount of work has followed on the problem of output regulation using internal model principle in more general

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¹In the paper [21], the case of time-varying \mathcal{S} is termed as quasi-DVI, but in this paper we do not make this distinction as we only consider the time-varying case and our results obviously hold when \mathcal{S} is stationary.

contexts and more recently in the context of discontinuous and hybrid systems, see [11], [12], [15], [19] and references therein. This paper could be seen as extending this principle for a class of nonsmooth systems expressed as DVIs.

In our results on output regulation, we will restrict ourselves to linear systems. The sets considered in the description of VIs for the exosystem and the plant are assumed to be the same but the mappings used to describe the relations could be different. We derive sufficient conditions under which there exists a control input that achieves output regulation while maintaining state constraints. In addition to the classical regulator synthesis equations, additional conditions are needed in our work to generate a dissipative relation between the multivalued part and the output regulation error. These additional conditions also guarantee that the closed-loop system is well-posed, that is, it admits a unique solution which is an important consideration for designing controllers for such class of systems. We study two cases for control synthesis depending on how much information is available to the controller. In the first case, it is assumed that the entire states of the plant and the exosystem are available and thus, a static controller is designed to achieve output regulation. In the second case, it is assumed that only the regulation error (which needs to converge to zero) is available and in that case a dynamic compensator is designed.

The rest of the paper is organized as follows: In Section II, we define the system class, formulate the problem of output regulation that we consider, and introduce some basic results from convex analysis. These results are used to develop a result on existence and uniqueness of solutions for proposed system class in Section III. The design of static state feedback is considered in Section IV, followed by the design of a dynamic compensator in Section V. The proofs of some intermediate results are collected in the Appendix.

II. PRELIMINARIES

A. Differential Variational Inequalities

Consider a set-valued mapping $\mathcal{S} : [0, \infty) \rightrightarrows \mathbb{R}^{d_s}$, and assume that $\mathcal{S}(t)$ is closed, convex, and nonempty, for each $t \geq 0$. The class of differential variational inequalities considered in this paper are described as follows:

$$\dot{x}(t) = f(t, x) + G\lambda(t) \quad (1a)$$

$$v(t) = Hx(t) + J\lambda(t), \quad v(t) \in \mathcal{S}(t), \quad (1b)$$

$$\langle v' - v(t), \lambda(t) \rangle \geq 0, \quad \forall v' \in \mathcal{S}(t). \quad (1c)$$

In the above equation $x(t) \in \mathbb{R}^n$ denotes the state, $\lambda(t), v(t) \in \mathbb{R}^{d_s}$, the vector field $f : [0, \infty) \times \mathbb{R}^n \rightarrow \mathbb{R}^n$ is absolutely continuous in first argument, and globally (and uniformly with respect to time) Lipschitz in second argument, $G \in \mathbb{R}^{n \times d_s}$, $H \in \mathbb{R}^{d_s \times n}$, $J \in \mathbb{R}^{d_s \times d_s}$ are constant matrices, and J is positive semidefinite.

In the standard references on variational inequalities, the multivalued mapping $\mathcal{S}(\cdot)$ is assumed to be stationary [13], [21]. To make connections with the standard formulation of evolution equations with time-varying domains [2], [20], it is seen that (1b), (1c) could be compactly written as:

$$\lambda(t) \in -\mathcal{N}_{\mathcal{S}(t)}(Hx(t) + J\lambda(t)), \quad (2)$$

where $\mathcal{N}_{\mathcal{S}(t)}(v(t))$ denotes the normal cone to a convex set at $v(t) \in \mathcal{S}(t)$, and is defined as:

$$\mathcal{N}_{\mathcal{S}(t)}(v(t)) := \{\lambda \in \mathbb{R}^{d_s} \mid \langle \lambda, v' - v(t) \rangle \geq 0, \forall v' \in \mathcal{S}(t)\},$$

and as convention we let $\mathcal{N}_{\mathcal{S}(t)}(v(t)) := \emptyset$, for $v(t) \notin \mathcal{S}(t)$.

In what follows, we will use the standard notations, int , and rint to denote the interior, and the relative interior of a set respectively. The domain, range, and kernel of an operator are denoted by dom , rge , and ker respectively.

B. Problem Formulation

As stated in the introduction, we basically consider two problems related to system class (1).

1) *Well-posedness of DVI* (1): First, we are interested in knowing under what conditions on the system dynamics, a unique solution exists in the following sense:

Definition 1: For each initial condition $x(0)$ satisfying $Hx(0) \in \mathcal{S}(0) + \text{rge } J$, there exists a locally absolutely continuous function $x : [0, \infty) \rightarrow \mathbb{R}^n$, such that $x(\cdot)$ satisfies (1a) for (Lebesgue-almost) every $t \geq 0$, and $Hx(t) \in \mathcal{S}(t) + \text{rge } J$.

2) *Output Regulation:* For this problem, we restrict ourselves to the case of linear vector fields, and the system class in particular is defined as follows:

$$\dot{x}(t) = Ax(t) + Bu(t) + Fx_r(t) + G\lambda(t) \quad (3a)$$

$$\lambda(t) \in -\mathcal{N}_{\mathcal{S}(t)}(Hx(t) + J\lambda(t)) \quad (3b)$$

where $x_r : [0, \infty) \rightarrow \mathbb{R}^{d_r}$ is the reference signal that is generated from the following equations:

$$\dot{x}_r(t) = A_r x_r(t) + G_r \lambda_r(t) \quad (4a)$$

$$\lambda_r(t) \in -\mathcal{N}_{\mathcal{S}_r(t)}(H_r x_r(t) + J_r \lambda_r(t)). \quad (4b)$$

The output regulation variable $w(\cdot)$ is defined as:

$$w(t) = Cx(t) + Dx_r(t). \quad (5)$$

It will be assumed throughout the paper that system (4) admits a solution (not necessarily unique) in the sense of Definition 1. We say that the output regulation is achieved if there exists a control input $u(\cdot)$ such that the following properties are satisfied:

- **Well-posedness:** For each initial condition $x(0)$ satisfying $Hx(0) \in \mathcal{S}(0) + \text{rge } J$, there exists a unique solution in the sense of Definition 1.
- **Regulation:** It holds that $\lim_{t \rightarrow \infty} w(t) = 0$.
- **Closed-loop stability:** The plant and controller dynamics have a globally asymptotically stable equilibrium at the origin when $x_r \equiv 0$.

C. Motivation

The solution theory for system (1) could be useful in many aspects since several electrical and mechanical systems are modeled using this framework. To motivate the output regulation, we mention two possible applications of the proposed problem.

1) *Viability Control and Regulation:* As first application, we consider the problem of finding a control input which maintains predefined constraints on the state trajectories of a dynamical system while achieving output regulation. Stated more precisely, suppose that we are given a plant described as:

$$\dot{x}(t) = Ax(t) + Bu(t) + Fx_r \quad (6)$$

and we would like to find a control $u(\cdot)$ which not only tracks a reference trajectory generated by the exosystem of form (4), but also results in the state satisfying the constraint that $Hx(t) \in \mathcal{S}(t)$, for all $t \geq 0$, where $\mathcal{S}(\cdot)$ is some predefined closed and convex set-valued map. This could be achieved by decomposing u as $u := u_{\text{reg}} + u_\lambda$, where we choose $u_\lambda(t)$ as the solution of the following variational inequality:

$$u_\lambda(t)^\top (v' - Hx(t)) \geq 0, \quad \forall v' \in \mathcal{S}(t). \quad (7)$$

This choice of control input transforms the plant equation (6) as follows:

$$\dot{x}(t) = Ax(t) + Bu_{\text{reg}}(t) + Bu_\lambda(t) + Fx_r(t). \quad (8)$$

For any $u_\lambda(\cdot)$ that satisfies (7), it now holds for the trajectories of the closed-loop system (8) that $v(t) := Hx(t) \in \mathcal{S}(t)$, provided that the system (8) is well-posed. The case of $\mathcal{S}(\cdot)$ being a time-varying polytope was also considered as a special case in our previous work [25]. In that case, (7) is formulated as a linear complementarity problem which could be solved very efficiently using standard softwares.

2) *Regulation in Power Converters:* A large number of electrical circuits with nonsmooth devices (diodes, switches, etc.), such as power converters, are modeled using complementarity relations which is a special kind of variational inequality when the set-valued map $\mathcal{S}(t) = \mathcal{K}$, where $\mathcal{K} \subseteq \mathbb{R}^{d_K}$ is some closed convex cone (see [1], [26] for examples). Let \mathcal{K}^* denote the dual cone to \mathcal{K} , defined as:

$$\mathcal{K}^* := \{\bar{v} \in \mathbb{R}^{d_K} \mid \langle \bar{v}, w \rangle \geq 0, \forall w \in \mathcal{K}\}.$$

Our framework allows us to consider the models of electrical systems of the following form:

$$\dot{x}(t) = Ax(t) + B_1 u_1(t) + F_1 x_r(t) + G\lambda(t) \quad (9a)$$

$$v(t) = Hx(t) + J\lambda(t) + F_2 x_r(t) + B_2 u_2(t) \quad (9b)$$

$$\mathcal{K} \ni v(t) \perp \lambda(t) \in \mathcal{K}^*, \quad (9c)$$

where $u_1(\cdot)$ and $u_2(\cdot)$ are control inputs that need to be designed to solve the regulation problem. Since \mathcal{K} is assumed to be a cone, the cone complementarity problem (9c) is equivalent to [13, Proposition 1.1.3]:

$$\lambda(t) \in -\mathcal{N}_{\mathcal{K}}(v(t)).$$

If we let $\bar{\mathcal{K}}(t) := \mathcal{K} - F_2 x_r(t) - B_2 u_2(t)$, so that $\bar{v}(t) \in \bar{\mathcal{K}}(t)$ if and only if $\bar{v}(t) + F_2 x_r(t) + B_2 u_2(t) \in \mathcal{K}$, then (9b), (9c) are equivalently written as:

$$\bar{v}(t) = Hx(t) + J\lambda(t)$$

$$\lambda(t) \in -\mathcal{N}_{\bar{\mathcal{K}}(t)}(\bar{v}(t))$$

and hence the system (9) is of the same form as (3).

D. Basic Results: Convex Analysis

In this section, we recall some basic results from convex analysis which are used in the subsequent sections for deriving main results of this paper. One can consult standard references, such as [22], for the results given here.

A set-valued map $\Phi(\cdot)$ is called *maximal monotone* if for each $x_1, x_2 \in \text{dom}(\Phi)$, and $y_i \in \Phi(x_i)$, $i = 1, 2$, we have $\langle y_2 - y_1, x_2 - x_1 \rangle \geq 0$, and the graph of Φ cannot be extended any further while satisfying the monotone property. We will not use the definition in its entirety. The monotone property is important and will be used repeatedly in analysis. Another important thing to know is that there is a vast literature on the solution theory of differential inclusions where the multivalued operator on the right-hand side is maximal monotone [3].

The following result allows us to draw connection between system (1a), (2) and the theory of maximal monotone operators.

Proposition 1: Consider a nonempty, closed and convex set \mathcal{S} and let $\psi_{\mathcal{S}}(\cdot)$ denote its indicator function, that is, $\psi_{\mathcal{S}}(v) = 0$, if $v \in \mathcal{S}$ and $\psi_{\mathcal{S}}(v) = +\infty$ otherwise; Then

- 1) it holds that $\partial\psi_{\mathcal{S}}(v) = \mathcal{N}_{\mathcal{S}}(v)$,
- 2) and $\mathcal{N}_{\mathcal{S}}(\cdot)$ is a maximal monotone operator.

In our approach, we would like to express (1) as a differential inclusion by replacing λ with a set-valued operator. In order to do that, one can see from (2) that we would need to define the “inverse” of the normal cone operator. The theory of conjugate functions (or Legendre-Fenchel transforms) [22, Chapter 11] allows us to make this connection.

Definition 2: For a function $g : \mathbb{R}^n \rightarrow [-\infty, +\infty]$, the function $g^* : \mathbb{R}^n \rightarrow [-\infty, +\infty]$ defined as:

$$g^*(\eta) := \sup_v \{\langle \eta, v \rangle - g(v)\}$$

is called the conjugate of g . For a closed convex set \mathcal{S} , the conjugate of the indicator function $\psi_{\mathcal{S}}(\cdot)$ is the support function $\sigma_{\mathcal{S}}(\cdot)$ defined as:

$$\sigma_{\mathcal{S}}(\eta) = \max_{v \in \mathcal{S}} \langle v, \eta \rangle.$$

We now recall the following fundamental result:

Proposition 2 ([22, Proposition 11.3]): For any proper, lower semicontinuous, convex function $g(\cdot)$, one has $\partial g^* = (\partial g)^{-1}$ and $\partial g = (\partial g^*)^{-1}$. That is,

$$\eta \in \partial g(v) \iff v \in \partial g^*(\eta). \quad (10)$$

In particular, for a closed and convex set \mathcal{S} :

$$\eta \in \mathcal{N}_{\mathcal{S}}(v) \iff v \in \partial \sigma_{\mathcal{S}}(\eta).$$

III. INCLUSION WITH MAXIMAL MONOTONE OPERATOR

There is a considerable amount of literature on the solution theory for differential inclusions, depending on the structure of the set-valued map on the right-hand side. One particular class of set-valued maps, which are interesting from the point of analysis and applications, are maximal monotone operators, and the solution theory for differential inclusions with such operators has been well-studied since the work of Brézis [3]. For our setup, such inclusions are of particular

interest because we will now show that, when the set $\mathcal{S}(t)$ is closed and convex valued, for each $t \geq 0$, then equation (1) can be equivalently written as a differential inclusion with time-varying maximal monotone operator plus a globally Lipschitz vector field on the right-hand side.

To see this, we use Propositions 1 and 2, and describe the relations in (1a), (1b), using a set-valued map for $\lambda(t)$ as follows:

$$\langle v' - v(t), \lambda(t) \rangle \geq 0, \quad \forall v' \in \mathcal{S}(t) \quad (11a)$$

$$\iff \lambda(t) \in -\partial\psi_{\mathcal{S}(t)}(Hx(t) + J\lambda(t)) \quad (11b)$$

$$\iff Hx(t) + J\lambda(t) \in \partial\sigma_{\mathcal{S}(t)}(-\lambda(t)) \quad (11c)$$

$$\iff Hx(t) \in (\partial\sigma_{\mathcal{S}(t)} + J)(-\lambda(t)) \quad (11d)$$

$$\iff \lambda(t) \in -(\partial\sigma_{\mathcal{S}(t)} + J)^{-1}(Hx(t)) \quad (11e)$$

Letting $\Phi(t, Hx(t)) := (\partial\sigma_{\mathcal{S}(t)} + J)^{-1}(Hx(t))$, system (1) can be equivalently written as the following differential inclusion:

$$\dot{x}(t) \in f(t, x) - G\Phi(t, Hx(t)). \quad (12)$$

It is an easy exercise to show that the operator $\Phi(t, \cdot)$ is maximal monotone for each $t \geq 0$ (see also proof of Lemma 1 in the Appendix) but it is not true in general that $G\Phi(t, H\cdot)$ is also maximal monotone. If it is assumed that $f(t, x) = Ax + u(t)$, and that the LTI system defined using the matrices (A, G, J, H) is passive and Φ is time-independent, then the maximal monotonicity of the multi-valued operator on the right-hand side of (12) was proven in [10]. Our goal in this section is to generalize this result for the class of systems (12), and the contribution of what follows could be seen in following two regards:

- A direct approach (different than [10]) to transform the right-hand side of (12) into a maximal monotone operator (with a minus sign) and a Lipschitz vector field, the solutions for which can be derived using existing results.
- Generalize the system class by addressing time-dependent sets and nonlinear vector fields.

A. Solution of Differential Inclusion (12)

Compared to the standard formulations of evolution equations with maximal monotone operators, the primary difficulty in studying the well-posedness of (12) is that the operator $G\Phi(t, H\cdot)$ may not necessarily be monotone for some arbitrary matrices G and H because multiplication with matrices does not preserve monotonicity. Secondly, the right-hand side depends on time and we need to impose some constraints on the evolution of the set-valued map $\mathcal{S}(\cdot)$ along with some regularity assumptions on $f(\cdot, x)$. The main result overcoming these difficulties is stated as follows:

Theorem 1: Assume that the following holds:

- (A1) The matrix J is positive semidefinite and there exists a symmetric positive definite matrix P such that $\ker(J + J^\top) \subseteq \ker(PG - H^\top)$.
- (A2) For each $t \geq 0$, the range space of H , denoted as $\text{rge } H$, cannot be separated from $\mathcal{S}(t) + \text{rge } J$.
- (A3) The mapping $\mathcal{S} : [0, \infty) \rightrightarrows \mathbb{R}^{d_s}$ is closed and convex valued with nonempty relative interior for each $t \geq 0$,

and varies in an absolutely continuous manner with time, that is, there exists an absolutely continuous function $\nu(\cdot) : [0, \infty) \rightarrow \mathbb{R}_+$, such that,

$$|d(v, \mathcal{S}(t_1)) - d(v, \mathcal{S}(t_2))| \leq |\nu(t_1) - \nu(t_2)|, \quad \forall t_1, t_2 \geq 0.$$

- (A4) The function $f(t, \cdot)$ is globally Lipschitz (uniformly in time), that is, there exists a constant $\mu > 0$ such that for each $t \geq 0$:

$$|f(t, x_1) - f(t, x_2)| \leq \mu|x_1 - x_2|, \quad \forall x_1, x_2 \in \mathbb{R}^n,$$

and $f(\cdot, x)$ is absolutely continuous for each $x \in \mathbb{R}^n$.

Then there exists a unique solution to (12), and hence (1), in the sense of Definition 1.

Discussions:

- 1) If $J = 0$, then (A1) basically implies that $PJ = H^\top$, which was the assumption used to deduce the maximal monotonicity of the multivalued operator in [5]. Also, if the quadruple (A, B, J, H) is passive, then the assumption (A1) automatically holds and this fact was also used in [10].
- 2) The constraint qualification (A2) is somewhat a standard assumption when dealing with problems on variational inequalities, and is introduced to preserve maximality under the composition function.
- 3) The bound on the variation of $\mathcal{S}(\cdot)$ is introduced to obtain absolutely continuous trajectories. It basically imposes the constraint that the Hausdorff distance between the sets $\mathcal{S}(t_1)$ and $\mathcal{S}(t_2)$ is relatively small for $|t_1 - t_2|$ sufficiently small. One could also relax the function $\nu(\cdot)$ to be continuous, or a function with locally bounded variation, in which case the resulting state trajectory will also be in the class of functions with locally bounded variation. However, this will only complicate the development as one has to interpret (12) as a measure differential inclusion. Nonetheless, we conjecture that most of the development carried out in the sequel will also carry over to that case.
- 4) The Lipschitz condition on the function $f(t, \cdot)$ is imposed because the inclusions with maximal monotone operators and Lipschitz perturbations are well-posed [3].

Proof of Theorem 1: The proof of Theorem 1 is based on several intermediate results which we will state as lemmas. The proofs of these lemmas are given in the Appendix.²

Lemma 1: For each $t \geq 0$, the operator $\Phi(t, \cdot) = (\partial\sigma_{\mathcal{S}(t)} + J)^{-1}(\cdot)$ is maximal monotone and $\text{dom } \Phi(t, \cdot) = \mathcal{S}(t) + \text{rge } J$.

Lemma 2: Consider $\eta_1, \eta_2 \in \Phi(t, Hx)$, then $\eta_1 - \eta_2 \in \ker(J + J^\top)$.

For each $\eta_\alpha \in \Phi(t, Hx)$ (with t and x fixed), let η^{im} denote the projection of η_α on the orthogonal complement of $\ker(J + J^\top)$, denoted as $\eta^{\text{im}} = \mathcal{P}_J(\eta_\alpha)$, then using Lemma 2, η^{im} is uniquely defined and we can write

$$\eta_\alpha := \eta^{\text{im}} + \eta_\alpha^{\text{ker}}$$

²In the proof of Theorem 1 and the Appendix, we will use the notation $\eta(t)$ to denote an element of the set $\Phi(t, Hx)$. From (11e), it is seen that the variable η and λ only differ by a sign change.

for some $\eta_\alpha^{\ker} \in \ker(J + J^\top)$. Since we have assumed that $\ker(J + J^\top) \subseteq \ker(PG - H^\top)$, we must have $G\eta_\alpha^{\ker} = P^{-1}H^\top\eta_\alpha^{\ker}$. This allows us to rewrite (12) as follows:

$$\begin{aligned}\dot{x}(t) &= f(t, x) - G\eta_\alpha^{\text{im}}(t) - P^{-1}H^\top\eta_\alpha^{\ker}(t) \\ &= f(t, x) + (P^{-1}H^\top - G)\mathcal{P}_J(\eta_\alpha(t)) - P^{-1}H^\top\eta_\alpha(t) \\ \eta_\alpha(t) &\in \Phi(t, Hx(t)).\end{aligned}\quad (13)$$

Let R denote the square root of the matrix P in (A1), so that R is also positive definite and symmetric. Introduce the coordinate transformation $z = Rx$, then in the new coordinates, (13) is written as:

$$\begin{aligned}\dot{z}(t) &= Rf(t, R^{-1}z) + (R^{-1}H^\top - RG)\mathcal{P}_J(\eta_\alpha(t)) \\ &\quad - R^{-1}H^\top\eta_\alpha(t) \\ \eta_\alpha(t) &\in \Phi(t, HR^{-1}z(t)).\end{aligned}\quad (14)$$

We will next use the following two results:

Lemma 3: The operator $\mathcal{P}_J(\Phi(t, H\cdot))$ is single-valued and Lipschitz continuous.

Lemma 4 ([22, Theorem 12.43]): The multivalued operator $R^{-1}H^\top\Phi(t, HR^{-1}\cdot)$ is maximal monotone, for each $t \geq 0$, if $\text{rge}(HR^{-1}) \cap \text{rint}(\text{dom}(\Phi(t, \cdot))) \neq \emptyset$, which holds in particular under the constraint qualification (A2).

As a result of these two lemmas, one can now write (14) as:

$$\dot{z}(t) \in g(t, z) - \Psi(t, z) \quad (15)$$

where $g(t, z) = Rf(t, R^{-1}z) - (R^{-1}H^\top - RG)\mathcal{P}_J(\eta_\alpha(t))$ is globally Lipschitz (in second argument) and $\Psi(t, z) = R^{-1}H^\top\Phi(t, HR^{-1}z(t))$ is maximal monotone for each $t \geq 0$. Finally, let

$$\bar{\Psi}(t, z) := \Psi(t, z) + g(t, z) - \bar{\mu}x,$$

where $\bar{\mu} > 0$ denotes the Lipschitz constant of $g(t, \cdot)$. It is easy to check that $\bar{\Psi}(t, z)$ is also maximal monotone. Inclusion (15) is now equivalent to:

$$\dot{z}(t) \in \bar{\mu}x - \bar{\Psi}(t, z). \quad (16)$$

One can now deduce the solution to (16) in the sense of Definition 1 by combining the results from [3, Chapter 3] and [18]. The precise arguments are worked out in the proof of following lemma given in the Appendix.

Lemma 5: For each $t \geq 0$, and there exists a unique locally absolutely continuous solution $z(\cdot)$, that satisfies (16) for almost every $t \geq 0$.

Since we have only introduced bijective operations in arriving from system (1) to (16), the conclusion also holds for system (1). ■

IV. FULL STATE FEEDBACK AND STATIC CONTROL

We will now use the results on the well-posedness of system (1) to solve the output regulation problem. In this section, it is assumed that all the states of the plant (1) and (4) are available for feedback and thus a control input with static state feedback can be designed which achieves the stability and regulation. In the formulation of our results, the following terminology is used: A quadruple of matrices

(A, B, C, D) is called *strictly passive* if there exist a scalar $\gamma > 0$ and a symmetric positive definite matrix P such that

$$\begin{bmatrix} A^\top P + PA + \gamma P & PB - C^\top \\ B^\top P - C & -(D + D^\top) \end{bmatrix} \leq 0. \quad (17)$$

Theorem 2: Consider systems (3), (4) under assumptions (A2) and (A3). Suppose that a matrix K renders the triplet $(A + BK, G, H, J)$ strictly passive, and that there exist matrices $\Pi \in \mathbb{R}^{n \times d_r}$ and $M \in \mathbb{R}^{d_u \times d_r}$ such that

$$\Pi A_r = A\Pi + BM + F \quad \text{and} \quad C\Pi + D = 0 \quad (18a)$$

$$\Pi G_r = G, \quad H\Pi = H_r \quad \text{and} \quad J_r = J. \quad (18b)$$

Then the output regulation problem is solvable with the following static feedback control law:

$$u(t) = Kx(t) + (M - K\Pi)x_r(t). \quad (19)$$

Remark 1: In the work of [14], the control law (19) was proposed to solve the output regulation problem in LTI systems, where Π and M were obtained as solution of (18a) only, and K is any matrix that makes $(A + BK)$ Hurwitz. The strict passivity requirement, and additional conditions on the matrix Π in (18b) are required in the well-posedness and stability analyses for the class of systems considered in this paper.

Proof: a) *Well-posedness:* With control input (19), the closed-loop system is written as

$$\begin{aligned}\dot{x}(t) &= (A + BK)x(t) + (F + BM - BK\Pi)x_r(t) + G\lambda(t) \\ \lambda &\in -\mathcal{N}_{S(t)}(Hx(t) + J\lambda(t)).\end{aligned}$$

Since $(A + BK, G, H, J)$ is assumed to be strictly passive, the matrix J is positive semidefinite and $\ker(PG - H^\top) \subseteq \ker(J + J^\top)$. All the remaining hypothesis of Theorem 1 hold by construction, and hence the closed-loop system exhibits a unique solution.

b) *Regulation:* Let Π be the matrix that satisfies (18) and introduce the variable $e = x - \Pi x_r$. The output regulation is achieved if we can show that $\lim_{t \rightarrow \infty} e(t) = 0$, since

$$\begin{aligned}w(t) &= Cx(t) + Dx_r(t) \\ &= Cx(t) - C\Pi x_r(t) = Ce(t).\end{aligned}$$

To show that $e(t) \rightarrow 0$ as $t \rightarrow \infty$, we observe that

$$\begin{aligned}\dot{e}(t) &= (A + BK)x(t) + (F + BM - BK\Pi)x_r(t) \\ &\quad + G\lambda(t) - \Pi A_r x_r(t) - \Pi G_r \lambda_r(t) \\ &= (A + BK)x(t) - \underbrace{(\Pi A_r - F - BM + BK\Pi)}_{=A\Pi} x_r(t) \\ &\quad + G\lambda(t) - \Pi G_r \lambda_r(t) \\ &= (A + BK)x(t) - (A + BK)\Pi x_r(t) \\ &\quad + G\lambda(t) - \Pi G_r \lambda_r(t) \\ &= (A + BK)e(t) + G(\lambda(t) - \lambda_r(t)).\end{aligned}$$

Now introduce the Lyapunov function $V(e) = e^\top P e$, so that the following holds for almost all $t \geq 0$:

$$\begin{aligned}\dot{V}(e(t)) &= e(t)^\top ((A + BK)^\top P + P(A + BK)) e(t) \\ &\quad + 2e(t)^\top PG(\lambda(t) - \lambda_r(t)) \\ &\leq -\gamma e(t)^\top P e(t) \\ &\quad + 2(\lambda(t) - \lambda_r(t), He(t) + J(\lambda(t) - \lambda_r(t)))\end{aligned}$$

where we used the passivity of $(A + BK, G, H, J)$ to arrive at the last inequality. Recalling that $He(t) = Hx(t) - H\Pi x_r(t) = H(x(t) - x_r(t))$, and $J_r = J$, the monotonicity of the normal cone operator leads to

$$\langle \lambda(t) - \lambda_r(t), H(x(t) - x_r(t)) + J(\lambda(t) - \lambda_r(t)) \rangle \leq 0.$$

It thus follows that $\dot{V}(e(t)) < 0$ for all $e(t) \neq 0$, and thus $e(t) \rightarrow 0$ as $t \rightarrow \infty$.

Closed-loop stabilization: Following the same calculations as above, it is seen that the derivative of $V(\cdot)$ along the dynamics of (3) with u in (19) satisfies

$$\dot{V}(x(t)) \leq -\gamma V(x(t)) + x(t)^\top P(F + B(M - K\Pi))x_r(t)$$

and it follows that $x(t) \rightarrow 0$ as $t \rightarrow \infty$, when $x_r \equiv 0$. ■

Example 1: As an illustration of Theorem 2, let us consider an example in the context of application discussed in §II-C.1. The plant to be controlled is a second order LTI system described by the equations

$$\dot{x}_1 = -0.1x_1 + x_2; \quad \dot{x}_2 = u.$$

The exosystem is defined as the following linear complementarity system:

$$\begin{aligned} \dot{x}_r &:= \begin{pmatrix} \dot{x}_{r1} \\ \dot{x}_{r2} \end{pmatrix} = \begin{bmatrix} -0.1 & 1 \\ -2 & 1 \end{bmatrix} x_r + \begin{bmatrix} 0 & 0 \\ -1 & 1 \end{bmatrix} \lambda_r \\ 0 &\leq \lambda_r \perp \begin{pmatrix} -x_{r2} \\ x_{r2} \end{pmatrix} + \begin{pmatrix} 1 \\ 1 \end{pmatrix} \geq 0. \end{aligned} \quad (20)$$

Consider the set $\mathcal{S} := \{z \in \mathbb{R} : z + 1 \geq 0\}$ and the matrix $H := \begin{bmatrix} 0 & -1 \\ 0 & 1 \end{bmatrix}$, then following the discussion in §II-C (see also [25, §5]), the relation (20) is equivalently expressed as $\lambda_r \in -\mathcal{N}_{\mathcal{S} \times \mathcal{S}}(Hx_r)$. We are interested in designing a control input u , such that $\lim_{t \rightarrow \infty} |x_2(t) - x_{r2}(t)| = 0$, and $\forall t \geq 0$, $|x_2(t)| \leq 1$, or equivalently $Hx(t) \in \mathcal{S} \times \mathcal{S}$. Verbally speaking, the exosystem has been chosen so that the plot of x_{r2} (versus time) resembles a sine wave clipped at the value 1, see Fig. 1. The control objective is to guarantee $|x_2(t)| \leq 1$ and that x_2 converges asymptotically to x_{r2} . Decomposing the input as $u := u_{\text{reg}} + u_\lambda$ results in the closed-loop system of the form (8). In the notation of Theorem 2, we let $\Pi = I_{2 \times 2}$, $P = \begin{bmatrix} 2 & 0 \\ 0 & 1 \end{bmatrix}$, $K = [-2 \ -2]$, and $M = [-2 \ 1]$, so that $u_{\text{reg}}(t) := -2x_1(t) - 2x_2(t) + 3x_{r2}(t)$ follows from (19). The discontinuous component of the input³ $u_\lambda := -u_{\lambda 1} + u_{\lambda 2}$ is obtained as a solution of the following complementarity problem:

$$0 \leq \begin{pmatrix} u_{\lambda 1} \\ u_{\lambda 2} \end{pmatrix} \perp \begin{pmatrix} -x_2 \\ x_2 \end{pmatrix} + \begin{pmatrix} 1 \\ 1 \end{pmatrix} \geq 0. \quad (21)$$

The results of the simulation are shown in Fig. 1.

³We are implicitly using the fact that the two constraints imposed in this problem, $x_2 \leq 1$ and $x_2 \geq -1$, are not active simultaneously. Thus, the complementarity formulation (21) ensures that $u_\lambda = -u_{\lambda 1}$ if $x_2 = 1$, and $u_\lambda = u_{\lambda 2}$ if $x_2 = -1$, otherwise $u_\lambda = 0$.

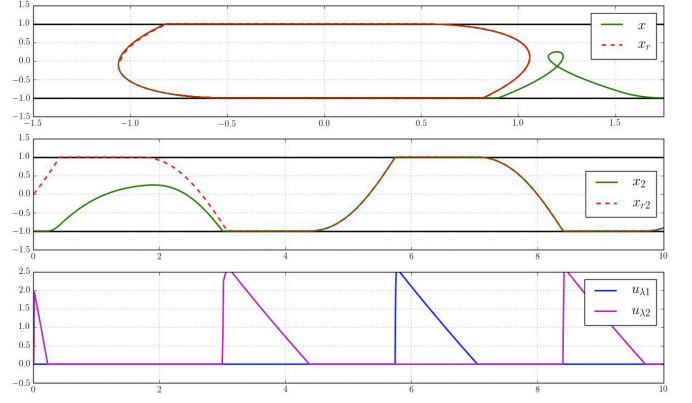


Fig. 1. The top plot shows the phase portrait of the trajectories of the plant and the exosystem. The middle plot confirms that x_2 converges to x_{r2} while staying within the set \mathcal{S} . The bottom plot shows the values of discontinuous component of the control input which only become nonzero when x is on the boundary of the set \mathcal{S} .

V. ERROR FEEDBACK AND DYNAMIC COMPENSATOR

In this section, it will no longer be assumed that the states $x(\cdot)$ and $x_r(\cdot)$ are available for feedback, but only the regulation error $w(\cdot)$ is available to the controller. Our approach is based on the *certainty equivalence principle* where we first design an estimator for the state variables $x(\cdot)$ and $x_r(\cdot)$ and then define the control law as a function of these estimates.

Towards this end, the estimator we propose is defined as follows:

$$\begin{aligned} \begin{pmatrix} \dot{\hat{x}} \\ \dot{\hat{x}}_r \end{pmatrix} &= \left[\begin{pmatrix} A & F \\ 0 & A_r \end{pmatrix} - \begin{pmatrix} L_0 \\ L_1 \end{pmatrix} \begin{pmatrix} C & D \end{pmatrix} \right] \begin{pmatrix} \hat{x} \\ \hat{x}_r \end{pmatrix} + \begin{pmatrix} L_0 \\ L_1 \end{pmatrix} w \\ &\quad + \begin{pmatrix} B \\ 0 \end{pmatrix} u + \begin{pmatrix} G & 0 \\ 0 & G_r \end{pmatrix} \begin{pmatrix} \hat{\lambda} \\ \hat{\lambda}_r \end{pmatrix} \end{aligned} \quad (22a)$$

$$\begin{pmatrix} \hat{\lambda} \\ \hat{\lambda}_r \end{pmatrix} \in -\mathcal{N}_{\mathcal{S}(t) \times \mathcal{S}(t)} \left(\overline{H} \begin{pmatrix} \hat{x} \\ \hat{x}_r \end{pmatrix} + \overline{J} \begin{pmatrix} \hat{\lambda} \\ \hat{\lambda}_r \end{pmatrix} \right), \quad (22b)$$

where the gain matrix $L := \begin{pmatrix} L_0 \\ L_1 \end{pmatrix}$ will be designed in the sequel, and the matrices $\overline{H}, \overline{J}$ are defined as follows:

$$\overline{H} := \begin{pmatrix} H & 0 \\ 0 & H_r \end{pmatrix}, \quad \overline{J} := \begin{pmatrix} J & 0 \\ 0 & J_r \end{pmatrix}.$$

For brevity, we have suppressed the time argument in (22), and will do so in the remainder of this section unless required. Let us also introduce the following notation:

$$\overline{A} := \begin{pmatrix} A & F \\ 0 & A_r \end{pmatrix}, \quad \overline{C} := \begin{pmatrix} C & D \end{pmatrix}, \quad \overline{G} := \begin{pmatrix} G & 0 \\ 0 & G_r \end{pmatrix}.$$

Theorem 3: Consider systems (3), (4) under assumptions **(A2)** and **(A3)**. Suppose that there exist a feedback matrix K and an injection matrix L that render the triplets $(A + BK, G, H, J)$ and $(\overline{A} - L\overline{C}, \overline{G}, \overline{H}, \overline{J})$ strictly passive, respectively. If there exist matrices $\Pi \in \mathbb{R}^{n \times d_r}$ and $M \in \mathbb{R}^{d_u \times d_r}$ that satisfy (18), then the output regulation problem is solved by letting

$$u(t) = K\hat{x}(t) + (M - K\Pi)\hat{x}_r(t). \quad (23)$$

Proof: Introduce the variable $\tilde{x} := x - \hat{x}$, then the closed-loop dynamics are *similar* to

$$\begin{pmatrix} \dot{\tilde{x}} \\ \dot{\hat{x}}_r \end{pmatrix} = \underbrace{\begin{pmatrix} A+BK & -BK & B(M-K\Pi) \\ 0 & A-L_0C & -F+L_0D \\ 0 & L_1C & A_r-L_1D \end{pmatrix}}_{:=A_{cl}} \begin{pmatrix} x \\ \tilde{x} \\ \hat{x}_r \end{pmatrix} + \underbrace{\begin{pmatrix} F \\ F-L_0D \\ L_1D \end{pmatrix}}_{:=F_{cl}} x_r + \underbrace{\begin{pmatrix} G & 0 & 0 \\ G & -G & 0 \\ 0 & 0 & G_r \end{pmatrix}}_{:=G_{cl}} \begin{pmatrix} \lambda \\ \hat{\lambda} \\ \hat{\lambda}_r \end{pmatrix} \quad (24a)$$

$$\begin{pmatrix} \lambda \\ \hat{\lambda} \\ \hat{\lambda}_r \end{pmatrix} \in -\mathcal{N}_{S(t) \times S(t) \times S(t)} \left(H_{cl} \begin{pmatrix} x \\ \tilde{x} \\ \hat{x}_r \end{pmatrix} + J_{cl} \begin{pmatrix} x \\ \tilde{x} \\ \hat{x}_r \end{pmatrix} \right), \quad (24b)$$

where we used the notation $H_{cl} := \begin{pmatrix} H & 0 & 0 \\ H & -H & 0 \\ 0 & 0 & H_r \end{pmatrix}$, and $J_{cl} := \begin{pmatrix} J & 0 & 0 \\ 0 & J & 0 \\ 0 & 0 & J_r \end{pmatrix}$.

Well-posedness: To show that the closed-loop system admits a unique solution, we follow the same procedure as in the proof of Theorem 2. That is, we find a symmetric positive definite matrix P_{cl} such that $\ker(P_{cl}G_{cl} - H_{cl}^\top) \subseteq \ker(J_{cl} + J_{cl}^\top)$. The matrix J_{cl} is positive semidefinite by construction. To find the matrix P_{cl} , it is noted that, by assumption, the quadruples $(A+BK, G, H, J)$ and $(\bar{A}-L\bar{C}, \bar{G}, \bar{H}, \bar{J})$ are strictly passive, so there exist symmetric positive definite matrices P, \bar{P} with dissipation constants $\gamma, \bar{\gamma}$, such that (17) holds. Now, partition \bar{P} as $\bar{P} := \begin{pmatrix} \bar{P}_{11} & \bar{P}_{12} \\ \bar{P}_{12}^\top & \bar{P}_{22} \end{pmatrix}$, then \bar{P}_{22} is a symmetric positive definite matrix, and $\bar{P}_{22}G_r = H_r^\top$. Thus, by letting

$$P_{cl} := \begin{bmatrix} 2P & -P & 0 \\ -P & P & 0 \\ 0 & 0 & \bar{P}_{22} \end{bmatrix}$$

it is easily checked that P_{cl} is symmetric, positive definite, and $\ker(P_{cl}G_{cl} - H_{cl}^\top) \subseteq \ker(J_{cl} + J_{cl}^\top)$.

Regulation: By letting $W := (-K \quad (M-K\Pi))$, it is seen that

$$A_{cl} = \begin{pmatrix} A+BK & BW \\ 0 & \bar{A}-L\bar{C} \end{pmatrix}$$

Define the regulation error as follows:

$$e := \begin{pmatrix} x - \Pi x_r \\ \tilde{x} \\ \hat{x}_r - x_r \end{pmatrix} =: \begin{pmatrix} e_x \\ \tilde{x} \\ e_r \end{pmatrix} =: \begin{pmatrix} e_x \\ e_\xi \end{pmatrix}, \quad (25)$$

then it can be shown using the equations in (18) that

$$\dot{e} = \begin{pmatrix} A+BK & BW \\ 0 & \bar{A}-L\bar{C} \end{pmatrix} e + \begin{pmatrix} G & 0 & 0 \\ 0 & G & 0 \\ 0 & 0 & G_r \end{pmatrix} \begin{pmatrix} \lambda - \lambda_r \\ \lambda - \hat{\lambda} \\ \lambda_r - \hat{\lambda}_r \end{pmatrix} \quad (26)$$

where λ, λ_r and $(\hat{\lambda}, \hat{\lambda}_r)$ are defined in (3b), (4b) and (22b), respectively.

Consider the Lyapunov function $V(e) = e^\top \begin{bmatrix} \alpha P & 0 \\ 0 & \beta \bar{P} \end{bmatrix} e$ for some $\alpha, \beta > 0$ to be specified later. The derivative of $V(\cdot)$ along the trajectories of the closed-loop system satisfies the following relations:

$$\begin{aligned} \dot{V}(e) &= \alpha e_x^\top (P(A+BK) + (A+BK)^\top P) e_x \\ &\quad + 2\alpha e_x^\top PBW e_\xi \\ &\quad + e_\xi^\top (\beta \bar{P}(\bar{A}-L\bar{C}) + (\bar{A}-L\bar{C})^\top \beta \bar{P}) e_\xi \\ &\quad + 2\alpha e_x^\top PG(\lambda - \lambda_r) + 2\beta e_\xi^\top \bar{P} \bar{G} \begin{pmatrix} \lambda - \hat{\lambda} \\ \lambda_r - \hat{\lambda}_r \end{pmatrix} \\ &\leq -\alpha \gamma e_x^\top P e_x - \beta \bar{\gamma} e_\xi^\top \bar{P} e_\xi + 2\alpha e_x^\top PBW e_\xi \\ &\quad + 2\alpha (\lambda - \lambda_r)^\top (H e_x + J(\lambda - \lambda_r)) \\ &\quad + 2\beta (\lambda - \hat{\lambda})^\top (H \tilde{x} + J(\lambda - \hat{\lambda})) \\ &\quad + 2\beta (\lambda_r - \hat{\lambda}_r)^\top (H_r e_r + J_r(\lambda_r - \hat{\lambda}_r)) \end{aligned}$$

where the last inequality is obtained using the passivity assumption on $(A+BK, G, H, J)$ and $(\bar{A}-L\bar{C}, \bar{G}, \bar{H}, \bar{J})$. Using the assumptions that $H\Pi = H_r$, and $J = J_r$, it now follows from the definition of the normal cone that

$$\begin{aligned} &(\lambda - \lambda_r)^\top (H e_x + J(\lambda - \lambda_r)) \\ &= \langle \lambda - \lambda_r, Hx - H\Pi x_r + J\lambda - J_r \lambda_r \rangle \\ &= \langle \lambda - \lambda_r, Hx + J\lambda - H_r x_r - J_r \lambda_r \rangle \leq 0 \end{aligned}$$

and using similar arguments,

$$\begin{aligned} &(\lambda - \hat{\lambda})^\top (H \tilde{x} + J(\lambda - \hat{\lambda})) \leq 0 \\ &(\lambda_r - \hat{\lambda}_r)^\top (H_r e_r + J_r(\lambda_r - \hat{\lambda}_r)) \leq 0. \end{aligned}$$

Plugging these relations in the expression for $\dot{V}(\cdot)$, and using the notation σ_{\min} to denote the smallest eigenvalue of a matrix and χ to denote the induced Euclidean matrix norm of PBW , we get

$$\begin{aligned} \dot{V}(e) &\leq -\alpha \gamma \sigma_{\min}(P) |e_x|^2 - \beta \bar{\gamma} \sigma_{\min}(\bar{P}) |e_\xi|^2 \\ &\quad + 2\alpha \chi |e_x| |e_\xi| \\ &\leq -\alpha \gamma \sigma_{\min}(P) |e_x|^2 - \beta \bar{\gamma} \sigma_{\min}(\bar{P}) |e_\xi|^2 + |e_x|^2 \\ &\quad + \alpha^2 \chi^2 |e_\xi|^2 \\ &= -(\alpha \gamma \sigma_{\min}(P) - 1) |e_x|^2 \\ &\quad - (\beta \bar{\gamma} \sigma_{\min}(\bar{P}) - \alpha^2 \chi^2) |e_\xi|^2. \end{aligned}$$

Thus, choosing α, β in the definition of the Lyapunov function $V(\cdot)$ such that $\alpha \gamma \sigma_{\min}(P) > 1$ and $\beta \bar{\gamma} \sigma_{\min}(\bar{P}) > \alpha^2 \chi^2$, makes $\dot{V}(\cdot)$ negative definite. In particular e_x converges to zero, from which it follows that $w = Cx + Dx_r = C(x - \Pi x_r) = Ce_x$ converges to zero.

Closed-loop stabilization: The closed-loop stabilization could be shown in exactly the same manner as above. The difference being, the derivative of the Lyapunov function $V(\cdot)$ is calculated along the trajectories of the dynamics of $(x, \tilde{x}, \hat{x}_r)$ given in (24). ■

VI. CONCLUSIONS

This paper studied the problem of output regulation in a certain class of nonsmooth dynamical systems that are modeled as differential variational inequalities. These systems

in particular model systems where states are constrained to evolve within some closed, convex and time-varying set. We first studied the conditions under which there exists a unique solution for such systems. The classical internal model principle was then used to derive conditions to synthesize a control law that achieves the desired objective. The analysis were based on using the Lyapunov methods in combination with monotonicity property of the normal cone operator to prove stability.

Several extensions are possible. The most interesting of which is to consider cases where the set-valued mapping $\mathcal{S}(\cdot)$ is not just time-dependent, but also state-dependent. This would allow us to model mechanical systems with impacts within our framework but deeper investigation is required for the synthesis of control in such cases.

APPENDIX

Proof of Lemma 1: First, it is noted that $\sigma_{\mathcal{S}(t)}$ is sublinear [22, Theorem 8.24], and hence a convex functional, so that $\partial\sigma_{\mathcal{S}(t)}$ is maximal monotone for each $t \geq 0$, and $\text{rint}(\text{dom } \partial\sigma_{\mathcal{S}(t)}) \neq \emptyset$ because $\mathcal{S}(t)$ is convex-valued and $\text{rint}(\mathcal{S}(t)) \neq \emptyset$. The matrix J define a monotone mapping, and being continuous, is also maximal monotone [22, Example 12.7]. Also, $\text{dom } J$ is \mathbb{R}^{d_s} . It now holds that $(\partial\sigma_{\mathcal{S}(t)} + J)$ is maximal monotone because $\text{rint}(\text{dom } \partial\sigma_{\mathcal{S}(t)}) \cap \text{rint}(\text{dom } J) \neq \emptyset$ [22, Corollary 12.44]. Hence, $(\partial\sigma_{\mathcal{S}(t)} + J)^{-1}$ is also maximal monotone, because the inverse operation preserves maximal monotonicity [22, Exercise 12.8(a)]. Also, using the fact that $\text{rge}(\mathcal{S}(t)) + J = \text{rge}(\mathcal{S}(t)) + \text{rge}(J)$, and that $\text{dom } \Phi(t, \cdot) = \text{rge}(\partial\sigma_{\mathcal{S}(t)} + J)$, the desired result follows. ■

Proof of Lemma 2: For $i = 1, 2$, consider $\eta_i \in (\partial\sigma_{\mathcal{S}(t)} + J)^{-1}(Hx)$, then $Hx - J\eta_i \in \partial\sigma_{\mathcal{S}(t)}(\eta_i)$. Since $\partial\sigma_{\mathcal{S}(t)}$ is monotone, we have

$$\langle Hx - J\eta_1 - Hx + J\eta_2, \eta_1 - \eta_2 \rangle \geq 0$$

or

$$\langle J(\eta_1 - \eta_2), \eta_1 - \eta_2 \rangle \leq 0.$$

It follows that $\eta_1 - \eta_2 \in \ker(J + J^\top)$, because J is positive semidefinite. ■

Proof of Lemma 3: From Lemma 2, it directly follows that the operator $\mathcal{P}_J(\Phi(t, H\cdot))$ is single-valued. Let $\eta^j := \mathcal{P}_J(\Phi(t, Hx^j))$, for $j = a, b$, so that $Hx^j - J\eta^j \in \partial\sigma_{\mathcal{S}}(\eta^j)$. Monotonicity of $\partial\sigma_{\mathcal{S}}$ gives

$$\langle Hx^a - J\eta^a - Hx^b + J\eta^b, \eta^a - \eta^b \rangle \geq 0$$

or equivalently,

$$\langle J(\eta^a - \eta^b), \eta^a - \eta^b \rangle \leq \langle H(x^a - x^b), \eta^a - \eta^b \rangle. \quad (27)$$

Since J is positive semidefinite, there exists $c > 0$, such that

$$|\mathcal{P}_J(\eta^a) - \mathcal{P}_J(\eta^b)| \leq c\langle J(\eta^a - \eta^b), \eta^a - \eta^b \rangle.$$

Assume now that, $\mathcal{P}_J(\Phi(t, H\cdot))$ is not Lipschitz, so for every $i \in \mathbb{N}$, there exist pairs (x_i^a, x_i^b) , $x_i^a \neq x_i^b$, and

$\eta_i^a \in \Phi(t, Hx_i^a)$, and $\eta_i^b \in \Phi(t, Hx_i^b)$, such that

$$\begin{aligned} i|x_i^a - x_i^b| &< |\mathcal{P}_J(\eta_i^a) - \mathcal{P}_J(\eta_i^b)| \\ &\leq c\langle J(\eta_i^a - \eta_i^b), \eta_i^a - \eta_i^b \rangle \\ &\leq c\langle H(x_i^a - x_i^b), \eta_i^a - \eta_i^b \rangle \\ &\leq c|x_i^a - x_i^b| \cdot |H^\top(\eta_i^a - \eta_i^b)|. \end{aligned}$$

Thus, we must have $|\eta_i^a - \eta_i^b| \geq |H^\top(\eta_i^a - \eta_i^b)|i$. Now dividing (27) by $|\eta_i^a - \eta_i^b|^2$, we get

$$\left\langle J \frac{(\eta_i^a - \eta_i^b)}{|\eta_i^a - \eta_i^b|}, \frac{\eta_i^a - \eta_i^b}{|\eta_i^a - \eta_i^b|} \right\rangle \leq \left\langle \frac{x_i^a - x_i^b}{|\eta_i^a - \eta_i^b|}, \frac{H^\top(\eta_i^a - \eta_i^b)}{|\eta_i^a - \eta_i^b|} \right\rangle.$$

Since the right-hand side converges to zero as i gets large, it follows that $\langle J(\eta_i^a - \eta_i^b), \eta_i^a - \eta_i^b \rangle$ converges to zero as well because J is positive semidefinite. But then $|\mathcal{P}_J(\eta_i^a) - \mathcal{P}_J(\eta_i^b)|$ converges to zero, which is a contradiction, and the desired claim follows. ■

Proof of Lemma 5: If $\bar{\mu} = 0$ in (16), then the result follows directly from [18, Theorem 3]. Next, for $i = 1, 2$, consider the differential inclusion

$$\dot{z}_i(t) \in -\bar{\Psi}(t, z_i) + g_i(t)$$

for some locally absolutely continuous functions $g_i(\cdot)$. It again follows from [18, Theorem 3] that there exists a unique solution $z_i(\cdot)$, which is locally absolutely continuous. It holds due to monotonicity of $\bar{\Psi}(t, \cdot)$ that

$$\begin{aligned} \frac{1}{2} \frac{d}{dt} |z_1(t) - z_2(t)|^2 &= \langle \dot{z}_1(t) - \dot{z}_2(t), z_1(t) - z_2(t) \rangle \\ &\leq \langle g_1(t) - g_2(t), z_1(t) - z_2(t) \rangle \\ &\leq |g_1(t) - g_2(t)| \cdot |z_1(t) - z_2(t)|. \end{aligned}$$

Letting $Z(t) := |z_1(t) - z_2(t)|^2$, the above inequality is rewritten as: $\dot{Z}(t) \leq 2|g_1(t) - g_2(t)|\sqrt{Z}(t)$. Applying the comparison lemma for solution of ODEs, we get

$$|z_1(t) - z_2(t)| \leq |z_1(0) - z_2(0)| + \int_0^t |g_1(s) - g_2(s)| ds. \quad (28)$$

To study the solutions of (16), consider a sequence of solutions with $z_1(t) = z(0)$, $t \geq 0$, and $z_{i+1}(\cdot)$, for $i \geq 1$ is obtained as a solution to following inclusion with initial condition $z_i(0) = z(0)$, $i \in \mathbb{N}$:

$$\dot{z}_{i+1}(t) \in -\bar{\Psi}(t, z_{i+1}) + \bar{\mu}z_i(t).$$

Then, from (28), we have, for each $t \geq 0$:

$$|z_{i+1}(t) - z_i(t)| \leq \int_0^t \bar{\mu}|z_i(s) - z_{i-1}(s)| ds$$

which through induction leads to:

$$|z_{i+1}(t) - z_i(t)| \leq \frac{(\bar{\mu}t)^i}{i!} \|z_2 - z_1\|_{\mathcal{L}_\infty}.$$

Thus, the sequence $\{z_i\}_{i=1}^\infty$ converges uniformly on every compact interval, and hence $\lim_{i \rightarrow \infty} z_i$ is the unique solution to system (16). ■

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